

Report on the National Aggregate Base Conference

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Vulcan Materials Co.

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AASHTO Subcommittee on Materials
Asheville, NC
August 5, 2008

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- Pennsylvania Aggregates and Concrete Association
- Tennessee Road Builders Association
- Texas Aggregates & Concrete Association
- Virginia Transportation Construction Alliance

Base Conference Program

- Overview of Current Design Techniques
- ICAR Mechanistic Design Model
- Life Cycle Cost Comparisons
- Optimizing Value and Performance of Aggregate Base Courses
- Compaction Requirements and Techniques
- Measurement and Testing (Density vs. Stiffness)
- Inverted Base Design and Performance
- Subbase for Rigid Pavements
- Drainage Layers Under Porous Pavements
- Texas Toll Road: High Performance Base Course Test Project

Overview of Current Design Techniques

Erol Tutemluer- University of Illinois

- Design approaches: empirical, mechanistic and mechanistic-empirical
- Mechanistic involves determining pavement responses due to loading through mathematical models tied to pavement responses through transfer functions
- AASHTO design procedures very conservative due to high No. 200 and low compaction in test road
- Design does not recognize excellent compressive strength and stress dependency of crushed aggregate base

ICAR Anisotropic Mechanistic Design Model

Dallas Little- Texas A&M University

- Unbound granular materials display anisotropic behavior (modulus values differ in the vertical and horizontal direction)
- The lower Poisson's ratio, the more anisotropic (AASHTO Road Test ~ 0.30)
- Anisotropy due to particle shape and methods of placement and densification

ICAR Anisotropic Mechanistic Design Model

Dallas Little- Texas A&M University

- Reductions in anisotropy
 - Decreases tensile strain at the bottom of the HMA layer
 - Reduces compressive strain at the top of subgrade
 - Reduces stresses at the top of the subgrade
 - Increases pavement performance

ICAR Anisotropic Mechanistic Design Model

Dallas Little- Texas A&M University

- Aggregate characteristics to reduce anisotropy
 - Larger top size, well-graded
 - Reduce flat/elongated particles
 - Increase angularity and texture
 - Control fines

Life Cycle Cost Comparisons

Bernie Kuta- FHWA

- Review of the elements and rationale for conducting life cycle cost analyses
- Demonstrated an analytical tool to provide a cost comparison of competing design alternatives producing equivalent benefits for the project being analyzed.

Optimizing Value and Performance

Don Powell- Vulcan Materials Co.

- Grading

- Use the largest top size available that can be accommodated by thickness
- Select a well graded material using the 0.45 power curve for a guide
- Select a maximum No. 200 level consistent with environmental concerns
- Use a grading that provides acceptable strength properties (CBR, triaxial or modulus)
- Use care if designing grading for permeability because of influence on strength.

Optimizing Value and Performance

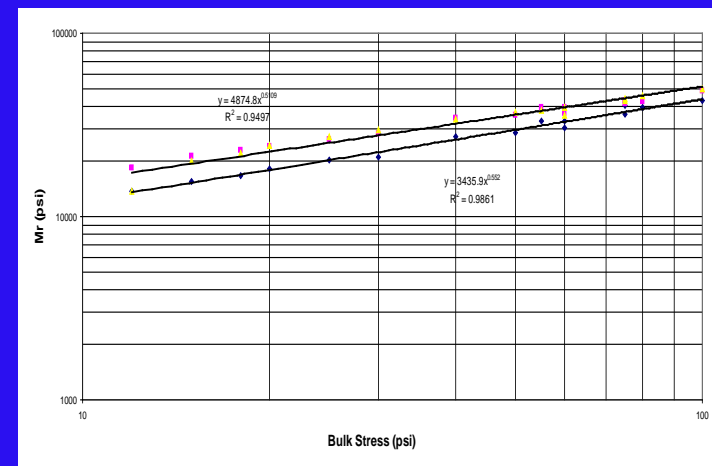
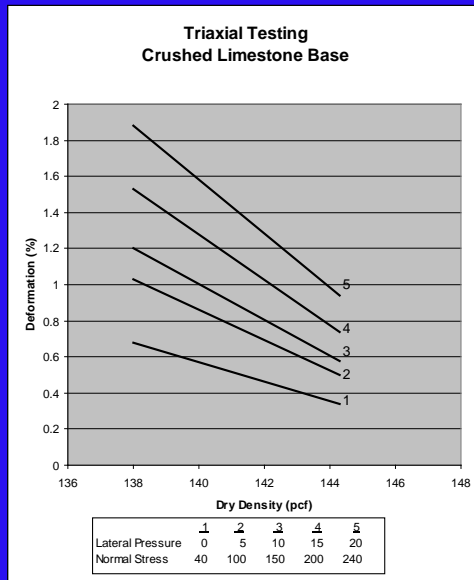
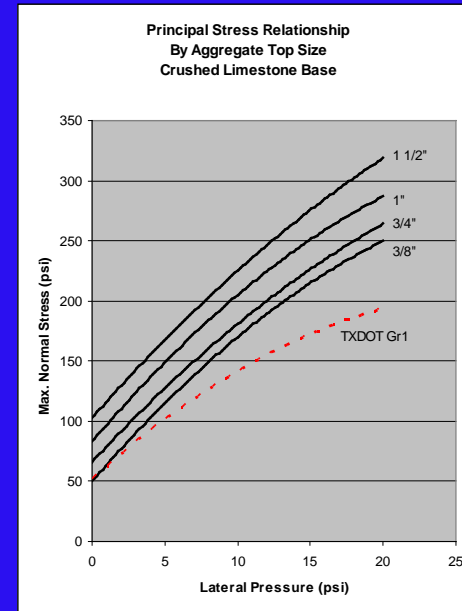
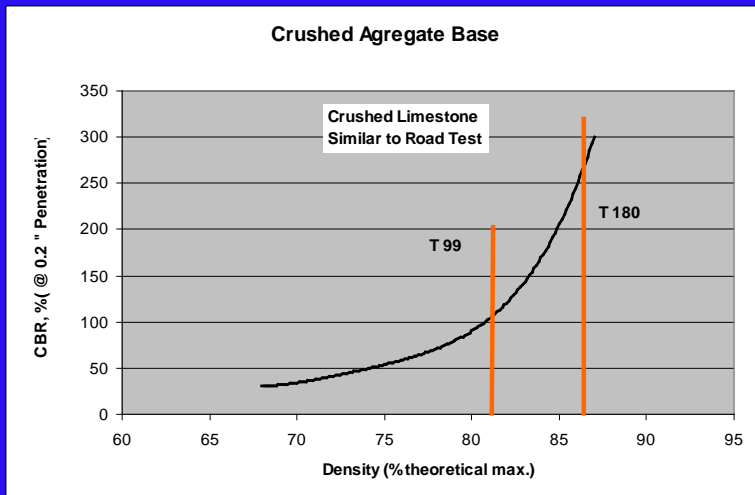
- Design Considerations
 - Insure subgrade strength and preparation is adequate
 - Require 100 % modified density in base
 - Single lift sections (max. 14 in.) if desired
 - Minimize thickness of HMA over base
 - Keep water out of the subgrade and base
 - Use larger top size grading
 - Require proper control and testing of placement

Optimizing Value and Performance

- Construction practices
 - Source approval for quality
 - Plant quality control for gradation and moisture
 - Establish the target density and optimum moisture (T-180)
 - Place with a spreader box to control thickness and minimize segregation
 - Avoid water additions on the roadway
 - Control compaction with nuclear gauge as placed & rolled
 - Seal quickly when sections are accepted

Optimizing Value and Performance

Impact of Density and Grading



Optimizing Value and Performance

- Benefits

- An economical alternative where available
- Can be placed in thick, single lifts
- Performs better when placed closer to the pavement surface
- Used in many of the excellent perpetual pavements still performing
- Performs best with a good subgrade
- Higher densities provide superior performance
- Low energy requirements (37 % less than HMA)

Compaction Requirements and Techniques

Chris Connelly- Bomag Corporation

- Reviewed the basic principles of compaction and the dynamic forces employed.
- Discussed the elements and potential of intelligent compaction and the opportunity to tie data acquisition with GPS for real time analyses.

Measurement and Testing (Density vs. Stiffness)

Ed Hall- Humboldt Mfg.

- Review of various test methods for density
- Nuclear gauge applications
- Proposed use of GeoGauge for measuring stiffness/modulus of pavement layers as opposed to density
- Field tests for stiffness ties to pavement design parameters

Inverted Base Design and Performance

John Cardosa- Georgia Crushed Stone Assn.

- Unbound aggregate base over a cement stabilized layer with reduced HMA thickness
- Georgia Test Road @ Lafarge Quarry
 - 6 in. GAB over 10 in. CTB
 - 2 in. HMA
 - Inverted sections show about 50 % less deflections using FWD
 - Standard section of 12.5 in. HMA over 12 in. GAB
 - After 65 % of design ESAL's, section shows no cracking

Inverted Base Design and Performance

John Cardosa- Georgia Crushed Stone Assn.

- LaGrange Bypass
 - Evaluate inverted base compared to a concrete paving section
 - Estimated 30 year LCCA savings of 20 %

Inverted Base Design and Performance

Randy Weingart- Luck Stone Corp.

- Virginia test sections on Hwy 659 Bypass to evaluate inverted base
- Joint effort with VDOT, FHWA and industry
- Project encompasses design, instrumentation, construction and monitoring
- Plan to incorporate deep-lift base construction techniques and intelligent compaction
- Compares current design practices with AASHTO MEPDG and the ICAR model
- Preliminary cost savings of 33 % over traditional design

Subbase for Rigid Pavements

Robert Rodden- ACPA

- Role of subbase/subgrade is not as critical for handling stresses as in flexible pavement
- Primary characteristics are uniformity, resist erosion, not susceptible to moisture
- Design of slab thickness not affected by subbase materials
- Don't want high modulus materials
- Reduce friction between slab and subbase
- Don't overdesign subbase for permeability (50 – 150 ft/day); daylight the subbase to ditches

Drainage Layers Under Pavements

John Yzenas- The Levy Co.

- Porous pavements
- Drainage layers under concrete pavement

Texas Toll Road- High Performance Base Course Test Project

Amit Basin- Texas A&M University

- SH 130 Austin Area
 - Variables are unbound and cement treated base, thick lift and large aggregate
 - Instrumented for permanent and resilient strain at various depths
 - Use a series of dynamic and long duration static loads

Level 1 Analysis Not Possible

- Finite Element Method not calibrated.

Unbound Layer - Layer #2

Unbound Material: Thickness(in): Last layer

Strength Properties ICM

Input Level:

Level 1:
 Level 2:
 Level 3:

Poisson's ratio:
Coefficient of lateral pressure, K_0 :


Analysis Type:

ICM Calculated Modulus
 ICM Inputs

User Input Modulus:

Seasonal input (design value)
 Representative value (design value)

Dg2k2

 Level 1 inputs utilize the stress dependent FEM which has not been calibrated with distress. Use of Level 1 is not recommended for design at this time.

OK

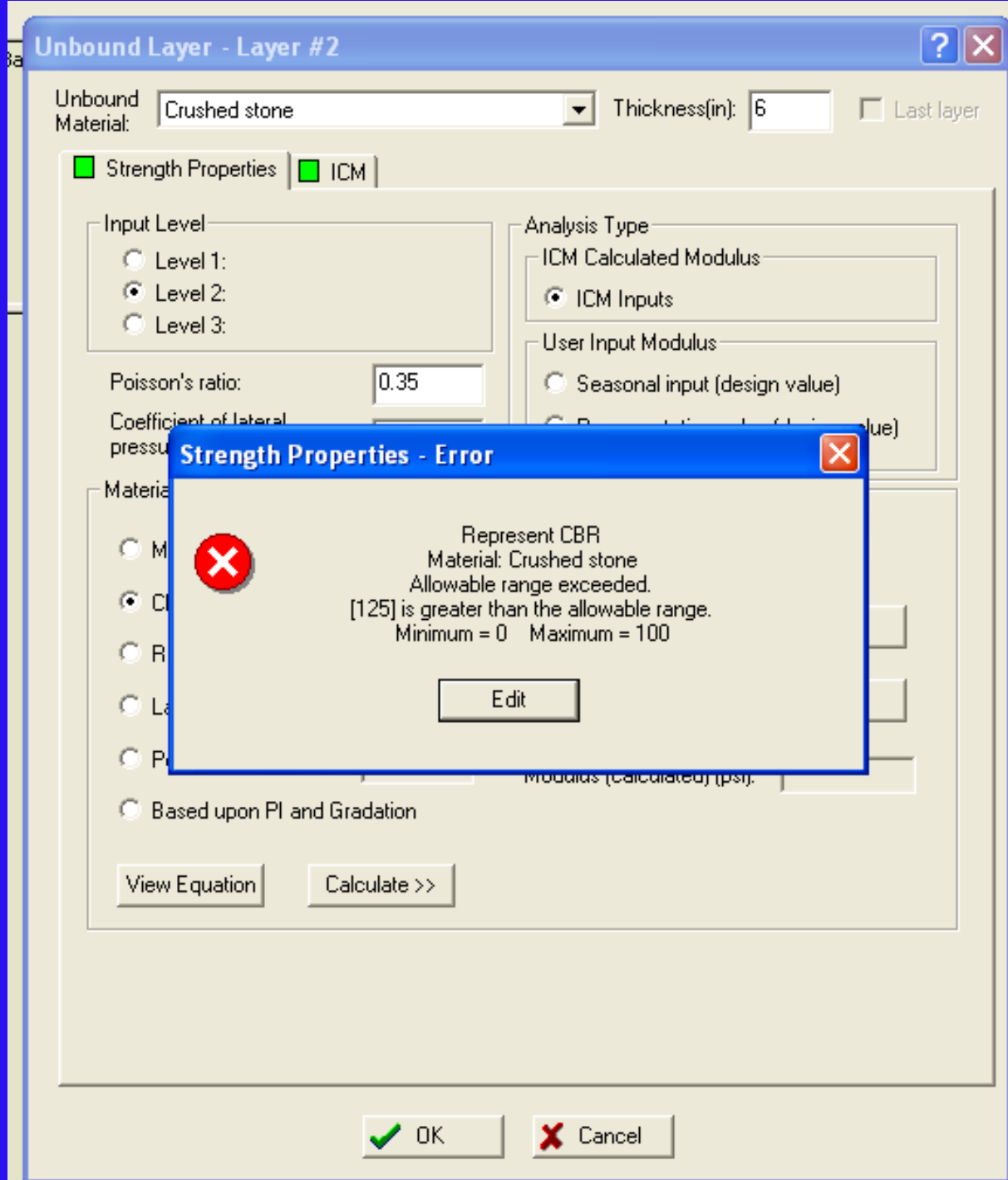
Penetration DCP (nr) Modulus (calculated) (psi):

Based upon PI and Gradation

OK Cancel

Limited Maximum CBR

- CBR max is 100.
- CBR can greatly exceed 100 for good quality crushed aggregate bases.





Project [C:\DG2002\Projects\Tech Managers F...

- General Information
- Site/Project Identification
- Analysis Parameters

Inputs

- Traffic
 - Traffic Volume Adjustment Factors
 - Monthly Adjustment
 - Vehicle Class Distribution
 - Hourly Truck Distribution
 - Traffic Growth Factor
 - Axle Load Distribution Factors
 - General Traffic Inputs
 - Number Axles/Truck
 - Axle Configuration
 - Wheelbase
- Climate
- Structure
 - Layers
 - Layer 1 - Asphalt concrete
 - Layer 2 - Crushed stone
 - Layer 3 - A-4
 - Thermal Cracking

Unbound Layer - Layer #2

Unbound Material: Thickness(in): Last layer

Strength Properties ICM

Input Level
 Level 1:
 Level 2:
 Level 3:

Analysis Type

 ICM Inputs

Poisson's ratio:
 Coefficient of lateral pressure, K_o:

User Input Modulus
 Seasonal input (design value)
 Representative value (design value)

Material Property
 Modulus (psi)
 CBR
 R - Value
 Layer Coefficient - a_i
 Penetration (DCP)
 Based upon PI and Gradation

Ranges from 35 to 80

Unified Classification

Status:

| Analysis | % Complete |
|------------------|------------|
| Traffic | 0% |
| Automatic | 0% |
| Thermal Cracking | 0% |
| Analysis | 0% |
| Summary | 0% |

Project Information:

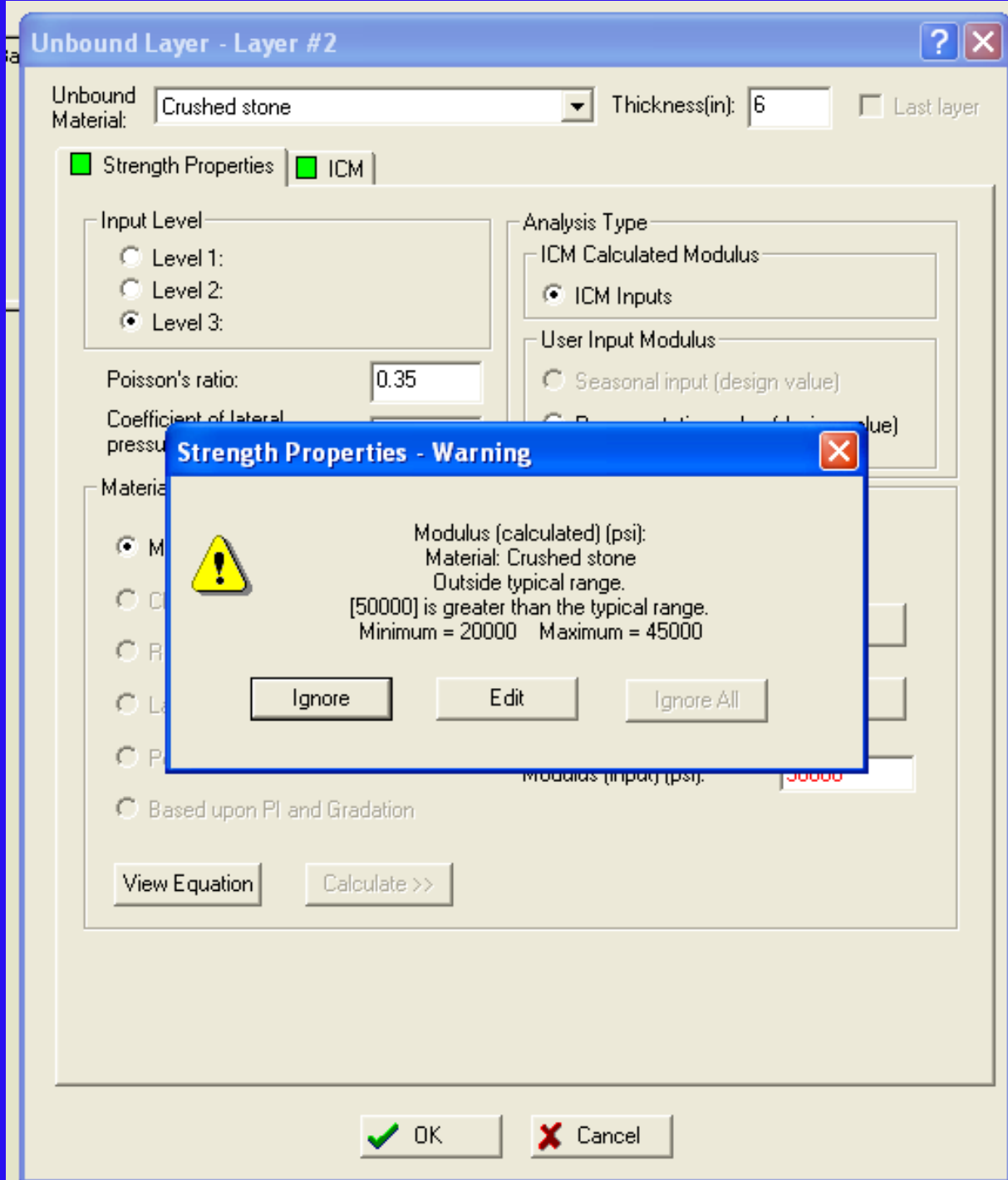
| Parameter | Value |
|---------------|--------------------------------|
| Project Name | New Flexible |
| Design Life | 10 Years |
| Project File | C:\DG2002\Projects\atlanta.icm |
| Creation Date | 9/2006 |
| Open Date | 10/2006 |
| ADTT | 4000 |

Information Box
 States CBR Ranges
 from 35 to 80

Run Analysis

Limited Maximum Resilient Modulus

- Modulus max = 45,000 psi.
- Greater modulus can exist when layer is placed closer to surface.



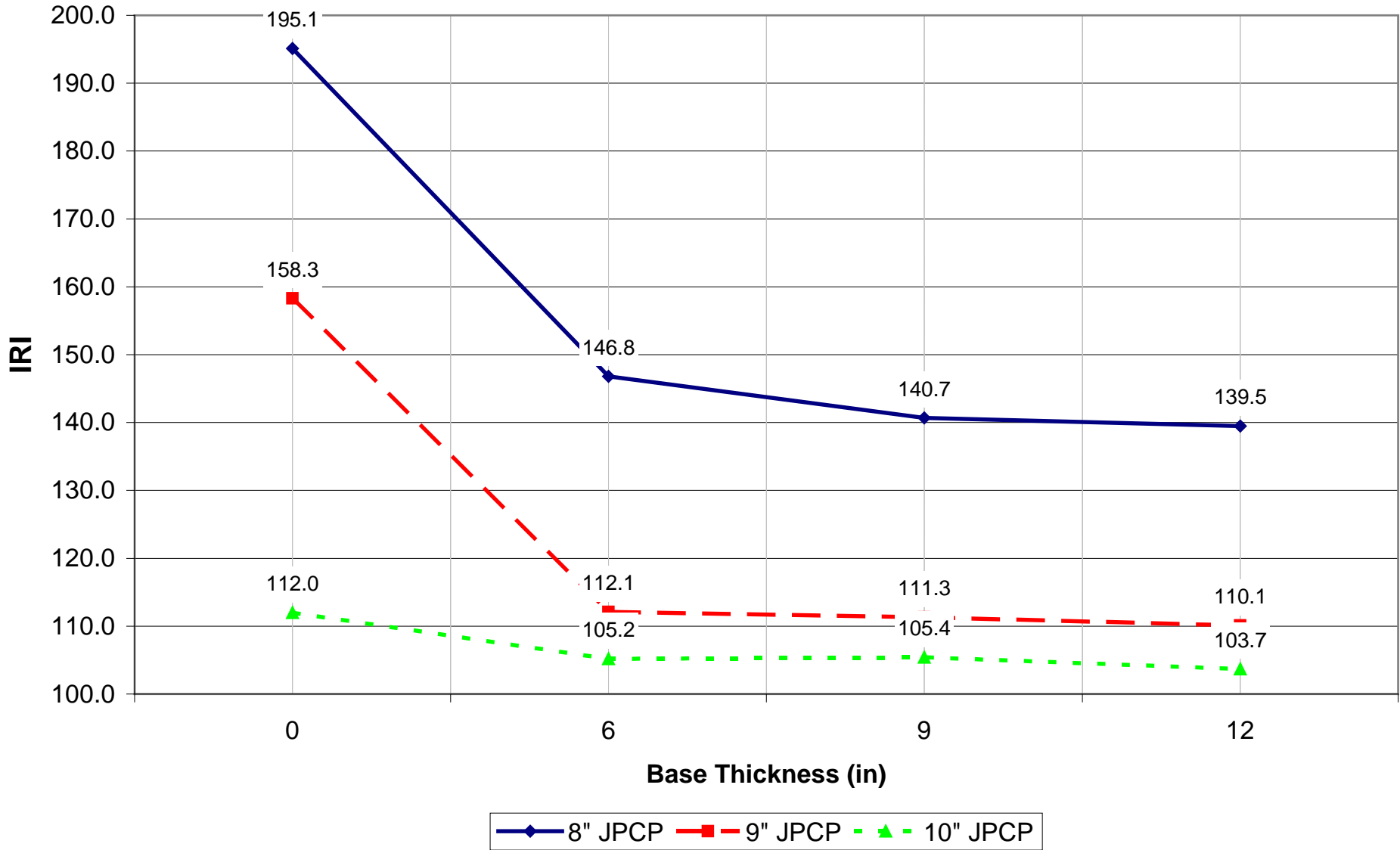
Rigid Pavement Analysis Example

- JPCP thickness
 - 8, 9, and 10 inches
- Base thickness
 - 0, 6, 9, and 12 inches
 - 40,000 psi Mr input
- A4 Subgrade
- 4,000 trucks per day
- Atlanta climate data

Rigid Pavement Analysis Example

| JCRP Thickness (in) | Base Thickness (in) | Terminal IRI (in/mi) | Transverse Cracking (% Slabs Cracked) | Mean Faulting (in) |
|---------------------|---------------------|----------------------|---------------------------------------|--------------------|
| 8 | 0 | 195.1 | 97.5 | 0.077 |
| 8 | 6 | 146.8 | 49.5 | 0.060 |
| 8 | 9 | 140.7 | 44.3 | 0.057 |
| 8 | 12 | 139.5 | 43.6 | 0.056 |
| 9 | 0 | 158.3 | 55.0 | 0.074 |
| 9 | 6 | 112.1 | 7.2 | 0.061 |
| 9 | 9 | 111.3 | 6.4 | 0.061 |
| 9 | 12 | 110.1 | 6.5 | 0.058 |
| 10 | 0 | 112.0 | 3.2 | 0.068 |
| 10 | 6 | 105.2 | 1.1 | 0.058 |
| 10 | 9 | 105.4 | 1.0 | 0.058 |
| 10 | 12 | 103.7 | 1.1 | 0.055 |

IRI



Transverse Cracking (% Slabs Cracked)

